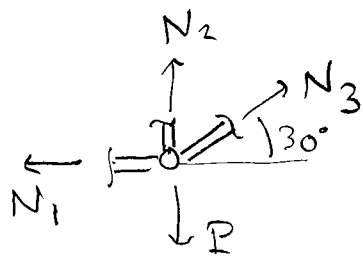


## Jämvikt för knutpunkt



$$\uparrow: N_2 + N_3 \underbrace{\sin 30^\circ}_{=1/2} - P = 0$$

$$\rightarrow: N_3 \underbrace{\cos 30^\circ}_{=\sqrt{3}/2} - N_1 = 0$$

$$\Rightarrow N_1 = N_3 \cdot \sqrt{3}/2, \quad N_2 = P - N_3/2 \quad (1)$$

## Konstitutiva samband

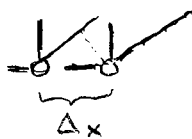
$$s_i = \frac{N_i L_i}{EA} \quad \text{för } i=1,2,3$$

$$\text{där } L_1 = L, \quad L_2 = 2L \cdot \tan(30^\circ) = \frac{2L}{\sqrt{3}}$$

$$L_3 = \frac{2L}{\cos(30^\circ)} = \frac{4L}{\sqrt{3}} \quad (2)$$

## Kompatibilitet

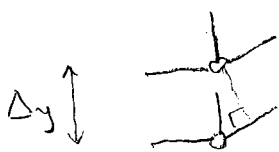
Horisontell förflyttning av knutpunkt  $\Delta_x$



$$\Rightarrow \begin{cases} \delta_1 = \Delta_x \\ \delta_2 = 0 \end{cases}$$

$$\delta_3 = -\Delta_x \cos(30^\circ) = -\Delta_x \sqrt{3}/2$$

Vertikal förflyttning av knutpunkt  $\Delta_y$



$$\Rightarrow \begin{cases} \delta_1 = 0 \\ \delta_2 = \Delta_y \\ \delta_3 = \Delta_y \sin(30^\circ) = \Delta_y/2 \end{cases}$$

$$\Rightarrow \delta_3 = -\delta_1 \cdot \sqrt{3}/2 + \delta_2/2 \quad (2) \Rightarrow \frac{N_3 \cdot 4}{\sqrt{3}} = -\frac{\sqrt{3}}{2} N_1 + \frac{1}{2} \frac{N_2 \cdot 2}{\sqrt{3}}$$

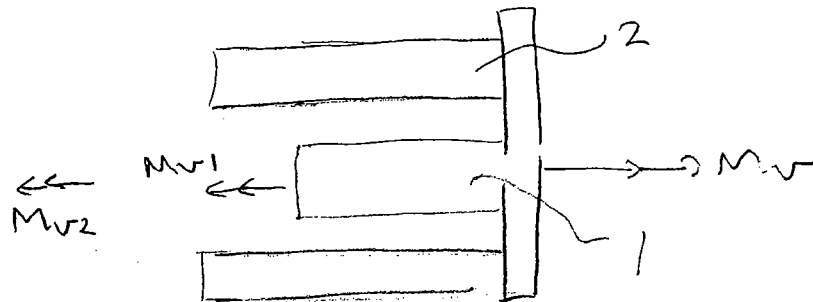
$$\stackrel{(1)}{\Rightarrow} N_3 \left( \frac{4}{\sqrt{3}} + \frac{\sqrt{3}}{2} \frac{\sqrt{3}}{2} + \frac{1}{\sqrt{3}} \frac{1}{2} \right) = \frac{1}{\sqrt{3}} \cdot P \Rightarrow N_3 \approx 0,172 \cdot P$$

$$\Rightarrow N_2 \approx 0,914 \cdot P, \quad N_1 \approx 0,149 \cdot P$$

⇒ Störst spänning i stång 2:

$$\sigma_2 = \frac{N_2}{A} \leq \sigma_{till} \Rightarrow A \geq \frac{N_2}{\sigma_{till}} = 9,14 [\text{mm}^2] //$$

a) Jämvikt för stel skiva



$$\rightarrow: M_v - M_{v1} - M_{v2} = 0 \Rightarrow$$

$$\boxed{M_{v1} = M_v - M_{v2}} \quad (1)$$

Deformationsvillkor

vridningen av axlarna lika stor

$$\Rightarrow \boxed{\varphi_1 = \varphi_2} \quad (2)$$

Konstitutiva samband

$$\varphi_1 = \frac{M_{v1} L}{G K_1} \quad \varphi_2 = \frac{M_{v2} L}{G K_2} \quad (3)$$

$$(3) \text{ i } (2) \Rightarrow \boxed{M_{v1} = M_{v2} \frac{K_1}{K_2}} \quad \text{insatt i (1)}$$

$$\Rightarrow M_{v2} \frac{K_1}{K_2} = M_v - M_{v2} \Rightarrow \boxed{M_{v2} = \frac{M_v K_2}{K_1 + K_2}}$$

$$\boxed{M_{v1} = \frac{M_v K_1}{K_1 + K_2}}$$

$$\text{Rotationen av skivan} = \varphi_1 = \varphi_2 = \boxed{\frac{M_v L}{G(K_1 + K_2)}}$$

$$\text{där } \begin{cases} K_1 = \frac{\pi}{2} b^4 \\ K_2 = \frac{\pi}{2} [(2b)^4 - a^4] \end{cases}$$

Med numeriska värden fås:

$$\varphi_1 = \varphi_2 \approx 2,3^\circ$$

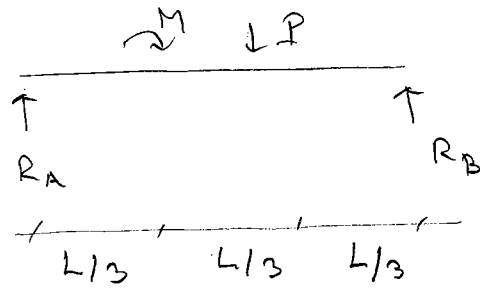
b) Största vridskjuvspänning fås enligt (6-14) i Lundh

$$\begin{cases} \tau_{\max,1} = \frac{2M_{v1} b}{\pi b^4} = \frac{2M_{v1}}{\pi b^3} \approx 324 \text{ MPa} \\ \tau_{\max,2} = \frac{2M_{v2} 2b}{\pi ((2b)^4 - a^4)} \approx 648 \text{ MPa} \end{cases}$$

$$\parallel M_{v1} = \frac{GK_1}{L} \varphi_1 = M_v \frac{K_1}{K_1 + K_2} \approx 509 \text{ Nm}$$

$$M_{v2} = M_v \frac{K_2}{K_1 + K_2} \approx 7091 \text{ Nm} \parallel$$

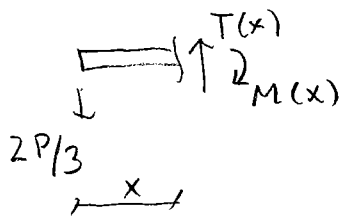
3) Jämvikt för hela balken



$$\begin{cases} \uparrow: R_A + R_B - P = 0 \\ \overline{\curvearrowright}: M + 2PL/3 - R_B \cdot L = 0 \end{cases}$$

$$\Rightarrow \begin{cases} R_B = M/L + 2P/3 = P + 2P/3 = 5P/3 \\ R_A = P - R_B = -2P/3 \end{cases}$$

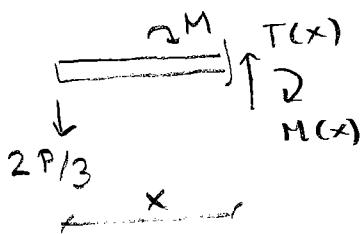
Snitta  $0 \leq x \leq L/3$



$$\uparrow: T(x) - 2P/3 = 0 \Rightarrow T(x) = 2P/3$$

$$\overline{\curvearrowright}: M(x) - 2P/3 \cdot x = 0 \Rightarrow M(x) = 2P/3 \cdot x$$

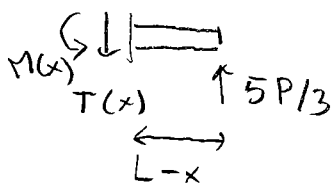
$L/3 \leq x \leq 2L/3$



$$\uparrow: T(x) - 2P/3 = 0 \Rightarrow T(x) = 2P/3$$

$$\overline{\curvearrowright}: M + M(x) - 2P/3 \cdot x = 0 \Rightarrow M(x) = 2P/3 \cdot x - M = P \left( \frac{2}{3}x - L \right)$$

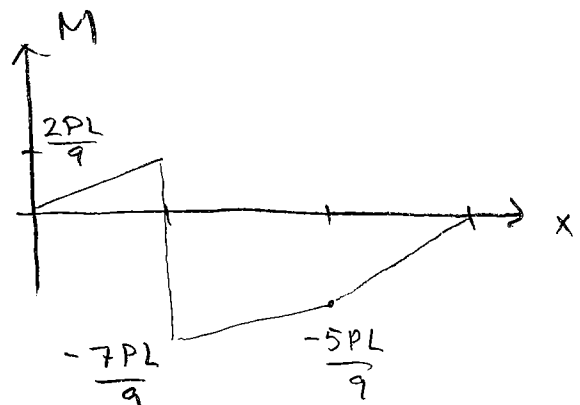
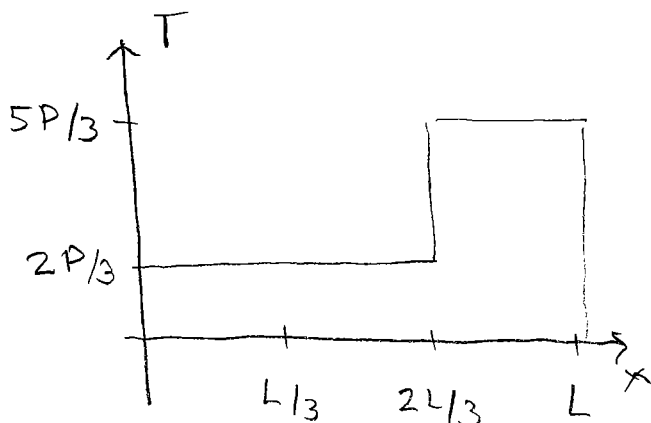
$2L/3 \leq x \leq L$

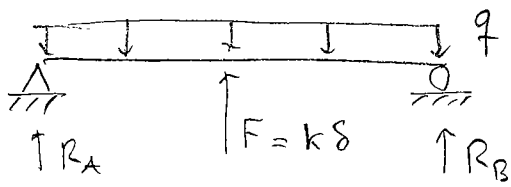


$$\uparrow: -T(x) + 5P/3 = 0 \Rightarrow T(x) = 5P/3$$

$$\overline{\curvearrowright}: -M(x) - 5P/3 (L-x) = 0 \Rightarrow$$

$$M(x) = 5P/3 \cdot (x - L)$$





Jämvikt:

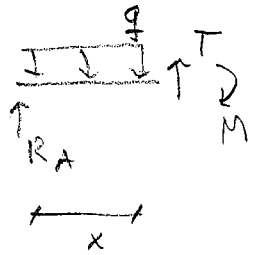
$$\uparrow: R_A + R_B + F - q \cdot 2L = 0$$

$$\overline{A}: q \cdot 2L^2 - F \cdot L - R_B \cdot 2L = 0$$

$$\Rightarrow R_B = qL - F/2, \quad R_A = R_B$$

Moment  $M(x)$  (av symmetriskäl är det tillräckligt att studera  $0 \leq x \leq L$ )

$0 \leq x \leq L$ :



$$\overline{x}: M(x) - qx^2/2 + R_A \cdot x = 0$$

$$\Rightarrow M(x) = (-qL + F/2)x + qx^2/2$$

$$\Rightarrow M'(x) = -qL + F/2 + qx$$

Störst (till belopp) moment fås för  $x=0$ ,  $x=L$  eller då  $M'(x)=0$

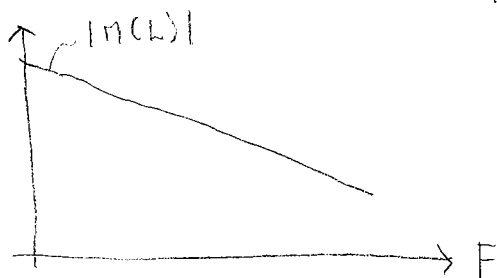
$$M(0) = 0$$

$$M(L) = (-qL + F/2)L + qL^2/2 = -qL^2/2 + FL/2 =$$

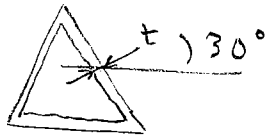
$$M'(x^*) = 0 \Rightarrow x^* = L - F/(2q) = L/2 (F - qL)$$

$$M(x^*) = \underbrace{(-qL + F/2) \left( L - \frac{F}{2q} \right)}_{-q \left( L - \frac{F}{2q} \right)^2} + \frac{q}{2} \left( L - \frac{F}{2q} \right)^2 =$$

$$= -q/2 \left( L - \frac{F}{2q} \right)^2 = -\frac{1}{2q} \left( qL - F/2 \right)^2$$



# Yttvöghetsmoment



$$I_y = \frac{h t^3}{12} + h \cdot t \cdot \left( \frac{\sqrt{3}}{2} h \cdot \frac{1}{3} \right)^2 +$$

$$+ 2 \cdot \left[ \frac{t}{\sqrt{3}/2} \left( h \cdot \frac{\sqrt{3}}{2} \right)^3 \frac{1}{12} + t \cdot h \left( h \frac{\sqrt{3}}{2} \left( \frac{1}{2} - \frac{1}{3} \right) \right)^2 \right]$$

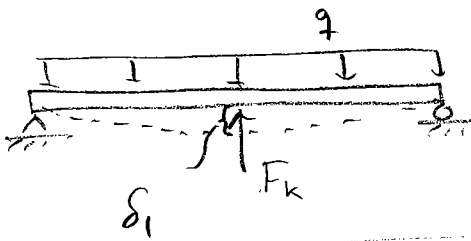
$$\approx 750225 \text{ mm}^4$$

## Max böjspänning

$$\sigma_{\max} = \frac{|M|_{\max} |z|_{\max}}{I_y} = \frac{7 PL/9 \cdot 2/3 \sqrt{3}/2 h}{I_y} \leq 200$$

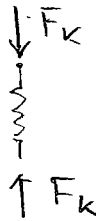
$$\Rightarrow P \leq 334 \text{ [N]} //$$

4)



nedböj i mitten förs från FS 6.3

$$\delta_1 = -\frac{F_k (2L)^3}{48EI} + \frac{q \cdot 5 \cdot (2L)^4}{384EI}$$



$$F_k = k \cdot \delta = \frac{1}{10} \frac{EI}{L^3} \delta$$

FS 6.4



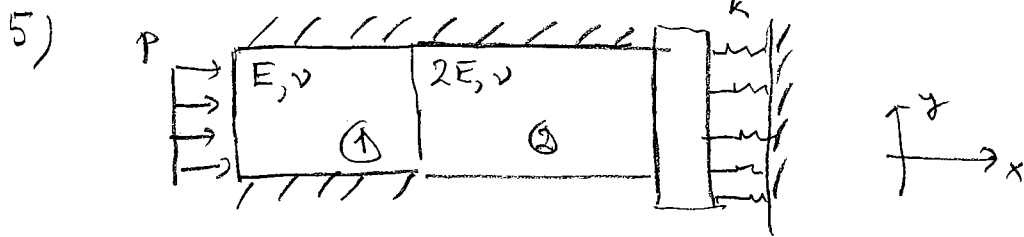
$$\delta_2 = \frac{F_k \cdot L^3}{3EI}$$

Kompatibilitet:

$$\delta = \delta_1 - \delta_2 \Rightarrow \frac{10L^3}{EI} \cdot F_k = \frac{L^3}{EI} \left[ -\frac{F_k}{6} + \frac{5}{24} qL - \frac{F_k}{3} \right]$$

$$\Rightarrow F_k = \frac{5qL}{244}$$

$$\Rightarrow \delta_2 = \frac{5}{244} qL \cdot \frac{L^3}{3EI} = \frac{5}{732} \frac{qL^4}{EI} \approx 0,00683 \frac{qL^4}{EI}$$



Del ①

$$\sigma_{x1} = -p, \quad \sigma_{y1} = ?, \quad \sigma_{z1} = 0$$

$$\varepsilon_{x1} = ?, \quad \varepsilon_{y1} = 0, \quad \varepsilon_{z1} = ?$$

Del ②

$$\sigma_{x2} = -p, \quad \sigma_{y2} = 0, \quad \sigma_{z2} = 0$$

$$\varepsilon_{x2} = ?, \quad \varepsilon_{y2} = ?, \quad \varepsilon_{z2} = ?$$

Hookes lag FS 8

$$\begin{aligned} \varepsilon_{y2} &= \frac{1}{2E} \left[ \sigma_{y2} - \nu (\sigma_{x2} + \sigma_{z2}) \right] = \frac{1}{2E} \left[ 0 - \nu \cdot (-p) \right] = \\ &= \frac{\nu \cdot p}{2E} \end{aligned}$$

$$\Rightarrow \delta_{y2} = \varepsilon_{y2} \cdot L = \frac{\nu \cdot p}{2E} \cdot 4 = 1/100 \Rightarrow$$

$$p = \frac{2E}{\nu \cdot 100} \approx 13,3 \text{ [GPa]}$$