

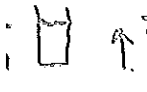
(2.8)

(2.13) $\nabla p = \rho(g - a) + \mu \nabla^2 v$

Ingen relativrörelse mellan elementen

$\nabla p = \rho(g - a)$

z-axeln uppåt $\Rightarrow \frac{dp}{dz} = \rho(-g - a)$ (1)

 $p_2 = 100 \text{ kPa}$, vi söker p_1

a) $a = 7g$

(1) $\Rightarrow \frac{dp}{dz} = \rho(-8g)$

$p_2 - p_1 = -8\rho g(z_2 - z_1)$

$p_1 = p_2 + 8\rho g(z_2 - z_1) =$

$= 100 \cdot 10^3 + 8 \cdot 1000 \cdot 9,81 \cdot 0,05 = 103,9 \text{ kPa}$

b) $a = -g$

(1) $\Rightarrow \frac{dp}{dz} = \rho \cdot 0$

$\Rightarrow p = \text{konst} \Rightarrow p_1 = p_2 = 100 \text{ kPa}$

c) $v = \text{konst} \Rightarrow a = 0$

(1) $\Rightarrow \frac{dp}{dz} = -\rho g$

$p_1 = p_2 + \rho g(z_2 - z_1) = 100,5 \text{ kPa}$

(samma som om muggen ställt still, dvs hydrostatiskt, om man bortser från vakeffekter. I verkligheten minst trycket p_2 också pga avlösning)

vatten 20°C: $\mu = 1,005 \cdot 10^{-3}$ $\rho = 1000$

luft 20°C: $\mu = 181 \cdot 10^{-6}$ $\rho = 1,2$

C_D fås vid dynamisk likf.

dvs $Re_m = Re_p$

$\frac{U_m D_m \rho_m}{\mu_m} = \frac{U_p D_p \rho_p}{\mu_p}$

$U_m = U_p \frac{D_p \rho_p \mu_m}{U_m D_m \rho_m \mu_p} =$

$= U_p \frac{D}{12} \frac{\rho_l}{\rho_v} \frac{\mu_v}{\mu_l} = U_p \cdot 0,8$

Ur diagram fås:

fördelning modellkast kraft

D 20 m/s 16 m/s 1,5 kW

25 m/s 20 m/s 2,4 kW

$F_D = \frac{1}{2} \rho_l A_r C_D U_p^2$ (1)

$F_m = \frac{1}{2} \rho_v A_r C_D U_m^2 \Rightarrow$

$C_D = \frac{2 F_m}{A_r \rho_v U_m^2}$ sätt in i (1)

$F_D = \frac{\rho_l}{\rho_v} \frac{A_r}{A_r} \left(\frac{U_p}{U_m}\right)^2 F_m =$

$= \frac{\rho_l}{\rho_v} \left(\frac{D}{D/12}\right)^2 \left(\frac{U_p}{U_m}\right)^2 F_m$

$= \frac{\rho_l}{\rho_v} 144 \left(\frac{U_p}{U_m}\right)^2 F_m$ (2)

(2) \Rightarrow

$F_D^{20} = 648 \text{ N}$

$F_D^{25} = 405 \text{ N}$

$P = F \cdot U$

$\Delta P = F_D^{25} \cdot 25 - F_D^{20} \cdot 20 =$

$8,1 \text{ kW}$

Givet: $L = 25 \text{ m}$ Olja av 30°C $\rho = 980 \text{ kg/m}^3$
 $d = 0,15 \text{ m}$
 $p_0 = 250 \text{ kPa}$ i centrum $\nu = 1,0 \cdot 10^{-6} \text{ m}^2/\text{s}$
 $p = 225 \text{ kPa}$

Lösning: $p_0 = p + \frac{\rho w_{\text{mitt}}^2}{2} \Rightarrow w_{\text{mitt}} = \sqrt{\frac{2(p_0 - p)}{\rho}} = 7,14 \text{ m/s}$

$Re = \frac{w \cdot d}{\nu} = k \cdot \frac{w_{\text{mitt}} \cdot d}{\nu} = k \cdot \frac{7,14 \cdot 0,15}{10^{-6}} = k \cdot 1,07 \cdot 10^6$

Strömningen är alltså turbulent med $k = 0,82$

$\dot{m} = \rho A w = 980 \cdot \frac{\pi \cdot 0,15^2}{4} \cdot 0,82 \cdot 7,14 = 101 \text{ kg/s}$

Svar: $\dot{m} = 100 \text{ kg/s}$



Givet: $x = 1 \text{ m}$, $\tau_{w1} = 8,2 \cdot 10^{-3} \text{ Pa}$
 $y = 4 \text{ mm}$, $U_{\infty 2} = 45 \text{ m/s}$
 utt av normalfästning $\Rightarrow \rho = 1,189 \text{ kg/m}^3$
 $\nu = 15,2 \cdot 10^{-6} \text{ m}^2/\text{s}$

Sort: a) $U_{\infty 2}$ b) $u_1(x, y)$
 c) τ_{w2} d) $u_2(x, y)$

Lösning: a) Bestäm om gränsskiktet är laminärt eller turbulent;

7,25) $\Rightarrow C_{f, \text{lam}} = \frac{0,664}{\sqrt{Re_x}} \Rightarrow$

$\Rightarrow \tau_{w, \text{lam}} = \frac{1}{2} \rho U_{\infty, \text{lam}}^2 \cdot 0,664 \sqrt{\frac{\nu}{U_{\infty, \text{lam}} \cdot x}} \Rightarrow$

$U_{\infty, \text{lam}} = \left(\tau_{w1} \frac{1}{0,664} \cdot \frac{2}{\rho} \sqrt{\frac{x}{\nu}} \right)^{1/2} = 3,05 \text{ m/s}$

$\Rightarrow Re_{x, \text{lam}} = \frac{U_{\infty, \text{lam}} \cdot x}{\nu} = 2,01 \cdot 10^5 \therefore \text{OK}$

43) $\Rightarrow C_{f, \text{turb}} = \frac{0,023}{Re_x^{1/4}} \Rightarrow \tau_{w, \text{turb}} = \frac{1}{2} \rho U_{\infty, \text{turb}}^2 \cdot 0,023 \left(\frac{\nu}{U_{\infty, \text{turb}} \cdot x} \right)^{1/4}$

$\Rightarrow U_{\infty, \text{turb}} = \left(\tau_{w1} \cdot \frac{2}{\rho} \cdot \frac{1}{0,023} \left(\frac{x}{\nu} \right)^{1/4} \right)^{2/3} = 1,63 \text{ m/s}$

$\Rightarrow Re_{x, \text{turb}} = \frac{U_{\infty, \text{turb}} \cdot x}{\nu} = 1,08 \cdot 10^5$

\therefore laminärt gränsskikt \Rightarrow

$U_{\infty 1} = U_{\infty, \text{lam}} = 3,05 \text{ m/s}$

b) lam. g.S. se Tab. 3.1 s. 397 med

$y \cdot \sqrt{\frac{U_{\infty, \text{lam}}}{\nu x}} = 0,498 \Rightarrow \frac{y}{U_{\infty, \text{lam}}} \approx 0,15$

eller interpolation $\Rightarrow u_1(x, y) = 0,46 U_{\infty 1}$

c) $U_{\infty 2} = 45 \text{ m/s} \Rightarrow Re_{x, 2} = \frac{U_{\infty 2} \cdot x}{\nu} = 3,0 \cdot 10^5$
 turbulent.

(7,43) $\Rightarrow \tau_{w, 2} = \frac{1}{2} \rho U_{\infty 2}^2 \cdot 0,023 \left(\frac{\nu}{U_{\infty 2} \cdot x} \right)^{1/4} = 3,87 \text{ Pa}$

d) (7,34) $\Rightarrow u^* = \frac{\tau_{w, 2}}{\rho \nu} = 1,0836 \text{ m/s}$

$\frac{u(x, y)}{u^*} = \frac{1}{\kappa} \ln \frac{y u^*}{\nu} + B$

med $\kappa = 0,41$ och $B = 5,0$

$\Rightarrow u_2(x, y) = 30,0 \text{ m/s}$

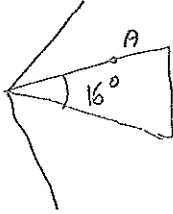
kont: $\frac{u^* y}{\nu} = \frac{1,0836 \cdot 0,001}{15,2 \cdot 10^{-6}} = 71$

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g) $Ma = 3$

Luft $\Rightarrow k = 1,4$

$P = 70 \text{ kPa}$



För $Ma_1 = 3$; $\theta = 8^\circ$ ger ekv (9.861)

$$\tan \theta = \frac{2 \cot \beta (Ma_1^2 \sin^2 \beta - 1)}{Ma_1^2 (k + \cos 2\beta) + 2}$$

Iterering $\Rightarrow \beta = 25,61^\circ$

$$\frac{P_A}{P_1} = \frac{1}{k+1} \cdot [2k \cdot Ma_1^2 \sin^2 \beta - (k-1)] \quad (9.83a)$$

$$\Rightarrow \underline{P_A = 126 \text{ kPa}}$$

1) En normal stat förmas

$$\Rightarrow P_B = P_{02}$$

Tabell B1 $\Rightarrow P_{01} = P / 0,0272 \Rightarrow 2574 \text{ kPa}$

Tabell B2, $Ma = 3 \Rightarrow P_{02} / P_{01} = 0,3283$

$$P_{02} = P_B = 0,3283 \cdot 2574 \text{ kPa} = \underline{845 \text{ kPa}}$$