

CHALMERS	Anonymous code	Points for question (to be filled in by teacher)	Consecutive page no. Löpande sid nr <u>1</u>
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Q1. (a) Advantages \Rightarrow efficiency
 \Rightarrow size (1)

Disadvantages \Rightarrow complicated control
 \Rightarrow component count (1)

(b) \Rightarrow switching losses (1)
 \Rightarrow conduction losses (1)

\Rightarrow the losses increase temperature of the MOSFET and reduce the component life time (1)

(c) unipolar excitation \Rightarrow Flyback, forward converter
 Bipolar excitation \Rightarrow half-bridge / full-bridge isolated (1)
 DC/DC Converter

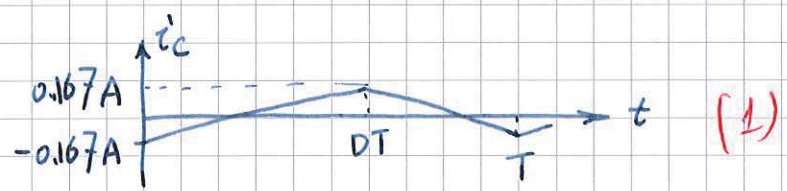
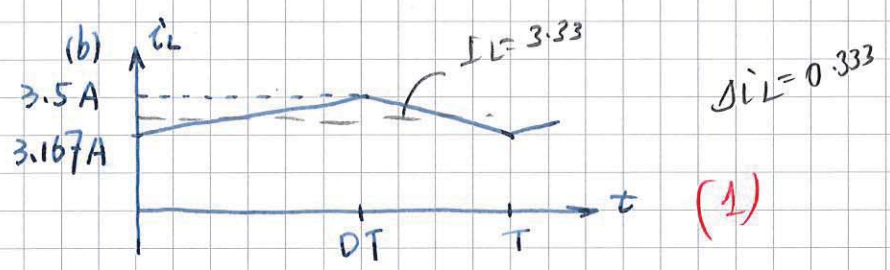
Bipolar excitation \Rightarrow larger working range due to higher $\pm \Delta B_{max}$ (1)

Q2. (a) $D = \frac{V_o}{V_d} = \frac{15V}{25V} = 0.6$ ($\Delta i_L = 10\% I_L \Rightarrow CCM$)

$I_L = I_o = \frac{P_o}{V_o} = 3.33A$

(1) $\Delta i_L = \frac{D(V_d - V_o)}{L \cdot f_{sw}}$ where $V_{oi} = V_d$ during DT_s
 $\Rightarrow V_L = V_d - V_o$
 $\Delta i_L = 10\% I_L$

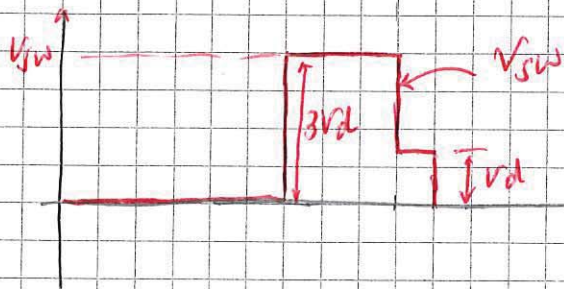
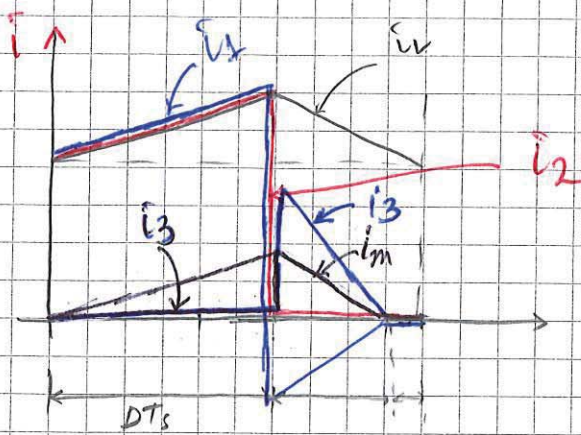
(1) $L = \frac{10 \cdot V_o \cdot D (V_d - V_o)}{P_o \cdot f_{sw}} = \frac{10 \cdot 15V \cdot 0.6 (25V - 15V)}{50W \cdot 20kHz}$
 $= 900 \mu H.$



(c) $\Delta V_o = \frac{Q}{C} = \frac{\Delta i_L}{8C f_{sw}} = 1\% V_o$

$C = \frac{100 \cdot \Delta i_L}{8 \cdot f_{sw} \cdot V_o} = \frac{100 \cdot 0.333A}{8 \cdot 20kHz \cdot 15V}$ (2)
 $= 13.89 \mu F.$

(d) During DT_s , $V_{sw} = 0$, i_m increases from 0. $i_3 = 0$ and $i_2 = i_L, i_1 = \frac{N_2}{N_1} i_2$
 During off period, i_m decreases to zero. $i_1 = -i_m$, $i_3 = \frac{N_1}{N_3} i_1, i_2 = 0$
 \Downarrow
 $V_{sw} = V_d + \frac{N_1}{N_3} V_d = 3V_d$
 $V_{sw} = V_d$ when $i_m = 0$



Q3. (a) Assume CCM.

$$V_o = \frac{N_3}{N_1} \cdot \frac{D}{1-D} \cdot V_d = 2 \cdot \frac{0.3}{1-0.3} \cdot 20V = 17.14V$$

$$I_o = \frac{V_o}{R} = \frac{17.14V}{20\Omega} = 0.86A$$

$$I_d = \frac{V_o \cdot I_o}{V_d} = \frac{17.14V \cdot 0.86A}{20V} = 0.73A$$

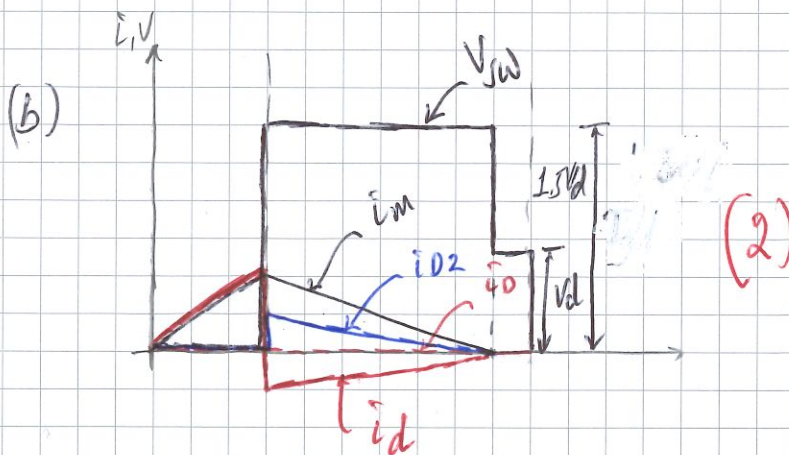
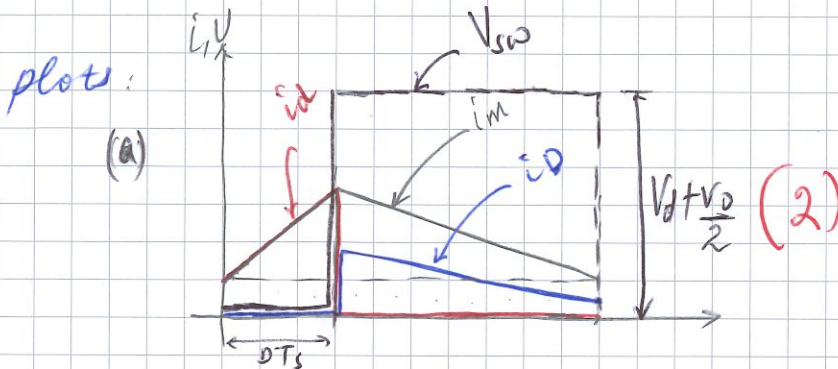
$$I_m = \frac{N_3}{N_1} I_o + I_d = 2 \cdot 0.86A + 0.73A = 2.45A \quad (2)$$

$$\Delta i_m = \frac{D \cdot V_d}{L_m \cdot f_{sw}} = \frac{0.3 \cdot 20V}{100\mu H \cdot 20kHz} = 3A$$

$$I_m > \frac{1}{2} \Delta i_m \quad CCM \quad V_o = 17.14V < \frac{N_2 \cdot V_d}{N_3} = 20$$

(b) When there is no load, $R_{load} = \infty$, the diode D_2 in the protection winding will conduct.

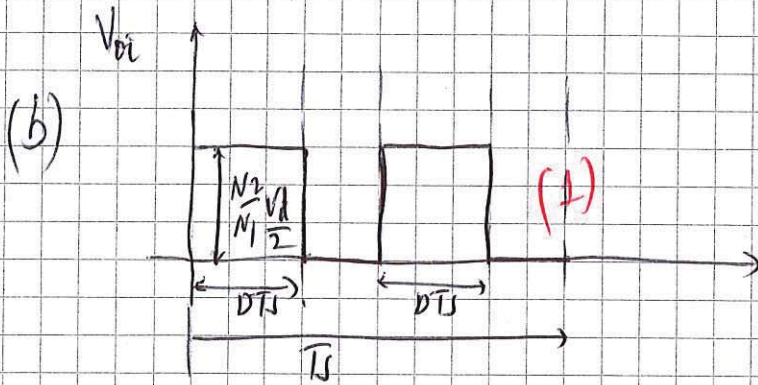
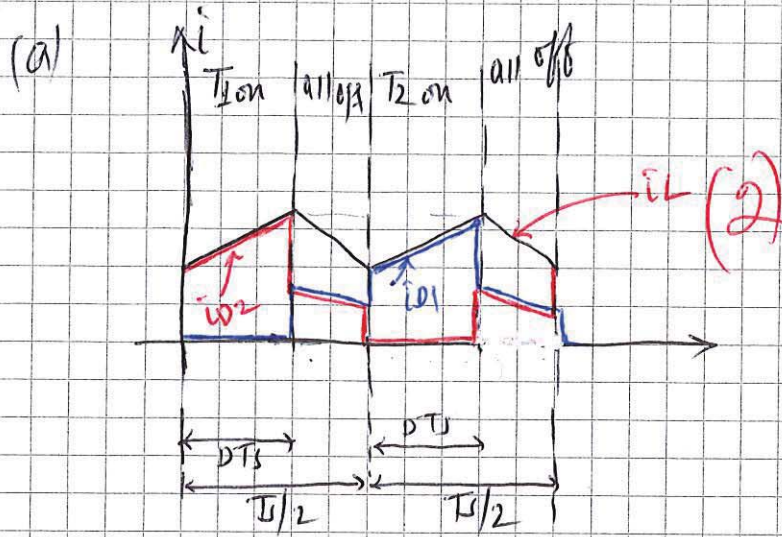
$$V_o = V_{o,max} = \frac{N_3}{N_3} V_d = 20V \quad (2)$$



(c) Flyback \Rightarrow core with air gap (1)
 \Rightarrow L_m small for higher magnetizing current
to increase energy stored (1)

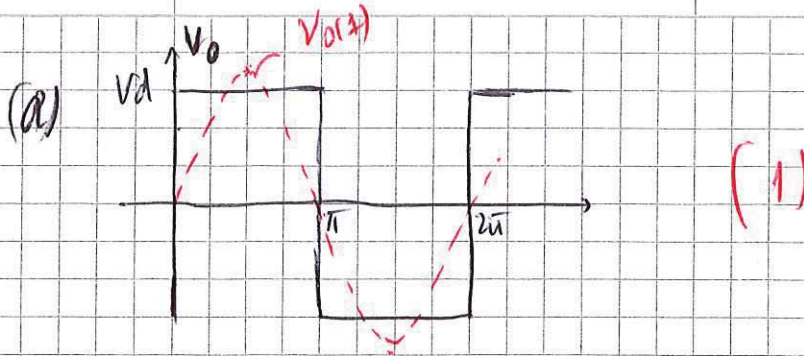
Forward \Rightarrow no air gap
 \Rightarrow L_m large to require small magnetizing
current

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$$V_0 = \frac{1}{T} \int V_{0i} dt = 2 \cdot D \cdot \frac{N_2 \cdot V_1}{N_1} \cdot \frac{1}{2}$$

$$\Rightarrow \frac{V_0}{V_1} = \frac{N_2 \cdot D}{N_1} \quad (1)$$



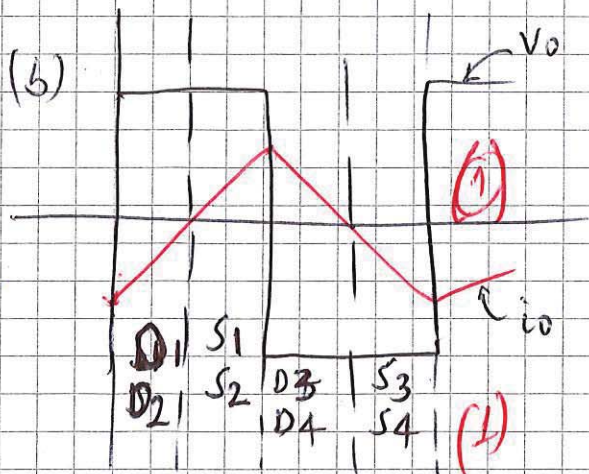
$$|\hat{v}_{o(n)}| = \frac{4}{\pi} \int_0^{\pi/2} v_d \sin(n\theta) d\theta = \frac{4v_d}{n\pi}, \text{ for odd } n.$$

$$\hat{v}_1 = \frac{4}{\pi} v_d = 382V \Rightarrow v_{o(1),RMS} = \frac{382}{\sqrt{2}} = 270.1 \text{ (1)}$$

$$v_{o,RMS} = \sqrt{\frac{1}{T} \int_0^T v_o^2 dt} = \sqrt{\frac{1}{T} \int_0^T v_d^2 dt} = v_d$$

$$\Rightarrow THD = \frac{\sqrt{v_{o(1),RMS}^2 - v_{o,RMS}^2}}{v_{o(1),RMS}} = \frac{\sqrt{v_d^2 - \left(\frac{4}{\pi} v_d\right)^2}}{\frac{4}{\pi} v_d} \times 100\%$$

$$\Rightarrow THD = \underline{\underline{48.34\%}} \text{ (1)}$$



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(c) 1 phase - ac-harmonics \Rightarrow 3, 5, 7, ...
 dc-harmonics \Rightarrow 2, 4, 6, ... (2)

3-phase - ac-harmonics \Rightarrow 5, 7, 11, 13
 dc-harmonics \Rightarrow 6, 12, ... (1)

(d) PWM advantages \Rightarrow Controlled output voltage
 \Rightarrow good current harmonics (1)

PWM disadvantages \Rightarrow higher switching losses
 \Rightarrow complicated control (1)

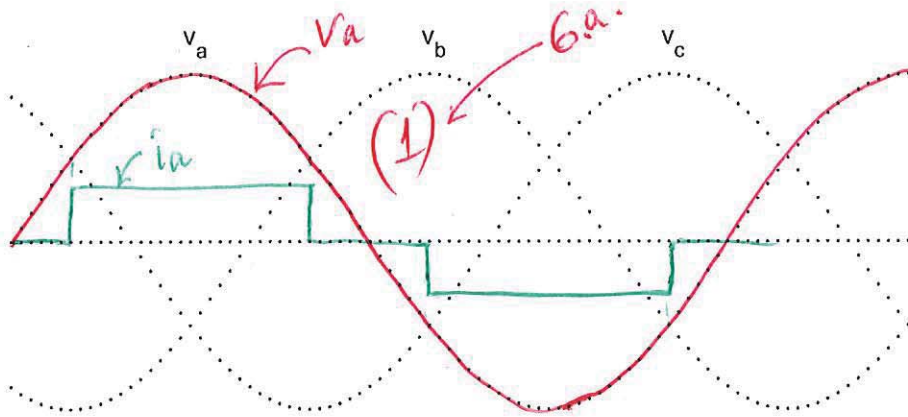
Dot paper for Question 6 (give a page number and put this paper together with your answer sheets if you use it for your answers. The distance between the dots in the voltage plots is 5° .)

6a.

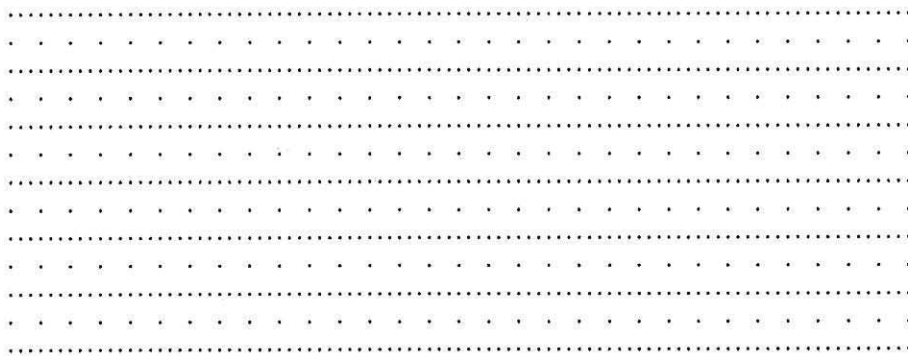
1) Phase-voltage plot for part 6.a.

(1)

$DPF = \cos(0^\circ) = 1$



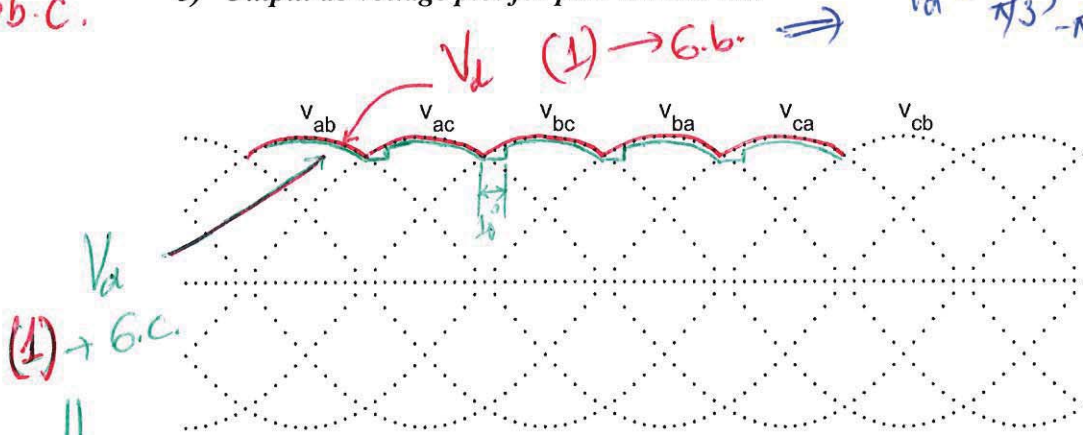
2) Phase-current plot for part 6.a.



6b.c.

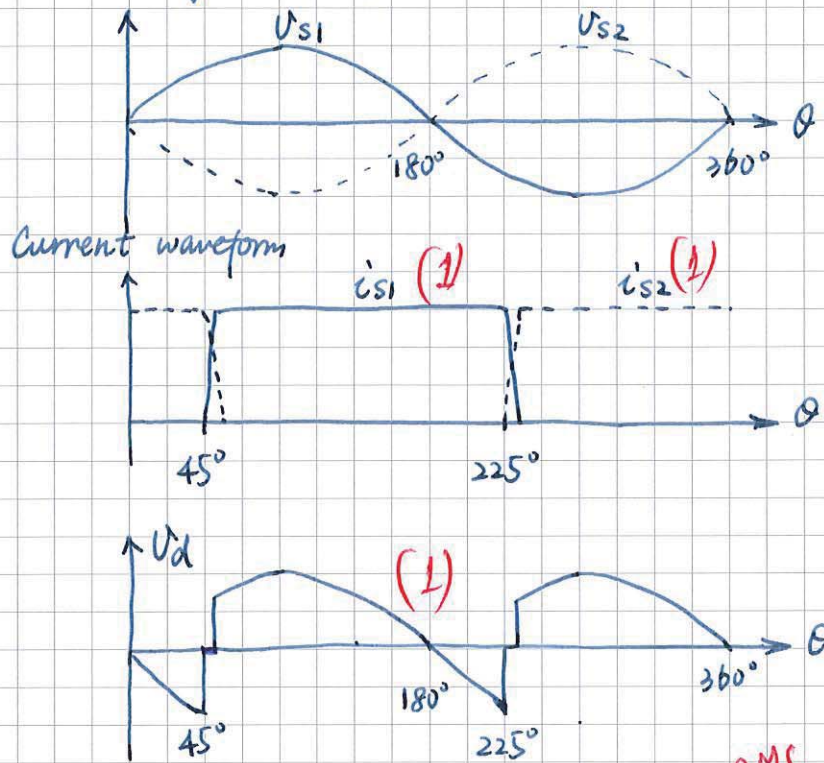
3) Output dc-voltage plot for part 6.b and 6.c.

$V_d = \frac{1}{\pi/3} \int_{-\pi/6}^{\pi/6} \sqrt{2} V_{LL} \cos \theta d\theta$ (1)
 $= \frac{3\sqrt{2}}{\pi} V_{LL} = 405V$



$DPF = \cos(2\pi/2) = \cos(5^\circ) = 0.9962$ (1)

Q7. (a) Voltage waveform.



$$(b) \quad u = \arccos \left(\cos \alpha - \frac{\omega L_s I_d}{\sqrt{2} V_s} \right) - \alpha$$

RMS

Peak

$$= \arccos \left(\cos 45^\circ - \frac{2 \cdot \pi \cdot 50 \text{ Hz} \cdot 5 \text{ mH} \cdot 10 \text{ A}}{187.8 \text{ V}} \right) - 45^\circ$$

$$= 6.43^\circ$$

Peak value (1)

$$V_d = \frac{2 \sqrt{2} V_s}{\pi} \cdot \cos \alpha - \frac{\omega L_s I_d}{\pi}$$

$$= \frac{2 \cdot 187.8 \text{ V}}{\pi} \cos 45^\circ - \frac{2 \cdot \pi \cdot 50 \text{ Hz} \cdot 5 \text{ mH} \cdot 10 \text{ A}}{\pi}$$

$$= 79.54 \text{ V} \quad (1)$$

To obtain a negative average voltage ($V_d < 0$),
the delay angle α should be larger than 87.6° . (1)