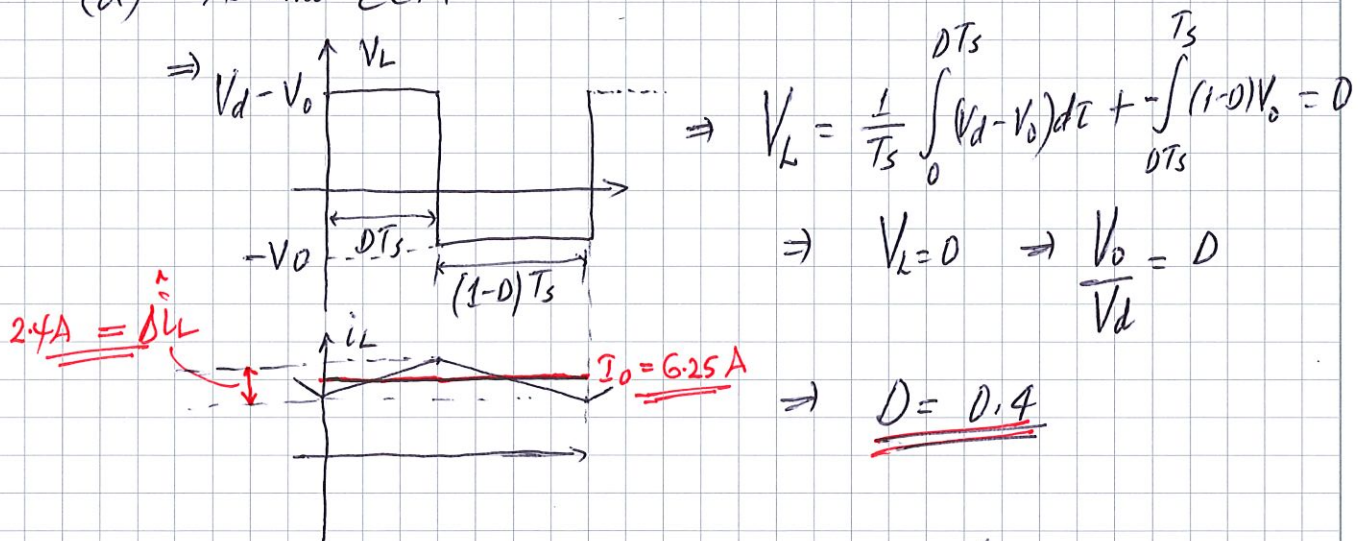


## Solution ENM061 Midterm Exam

Q#1. Refer to the lecture notes for the answers.

Q#2.  $V_o = 8V$        $f_{sw} = 20 \text{ kHz} \Rightarrow T_s = \frac{1}{f_{sw}}$   
 $V_d = 20V$        $L = 100 \mu\text{H}$   
 $P_o = 50W$        $C = 500 \mu\text{F}$

(a) Assume CCM



during switch on,  $v_L = V_d - V_o = 12V = \frac{L \Delta i_L}{DT_s}$

$\Rightarrow \Delta i_L = \frac{DT_s (V_d - V_o)}{L} = \frac{(0.4)(12)}{20(10^{-3}) \cdot 100(10^{-6})} = \underline{\underline{2.4 \text{ A}}}$

$I_L = \frac{1}{T_s} \int_0^{T_s} i_L(t) dt = I_o = \frac{P_o}{V_o} = \frac{50}{8} \text{ A} = \underline{\underline{6.25 \text{ A}}}$

$\frac{\Delta i_L}{2} < I_L \Rightarrow$  the assumption of CCM is correct

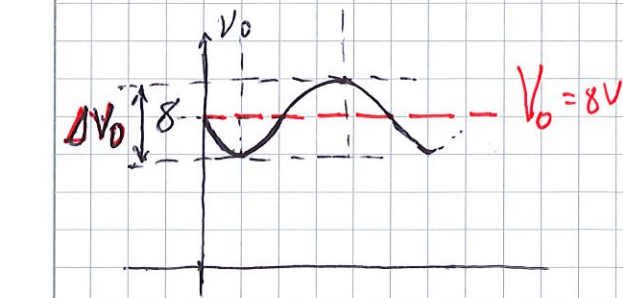
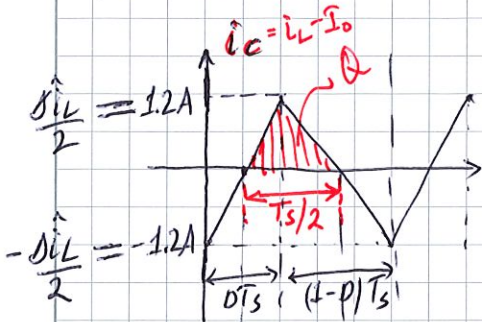
(b)  $I_o = 6.25 \text{ A}$  from part (a)

From energy conservation (100% efficiency of converter)

$P_{in} = P_o \Rightarrow V_d I_d = P_o$

$\Rightarrow I_d = \frac{50}{20} \text{ A} = \underline{\underline{2.5 \text{ A}}}$

(c)  $i_{c(t)} = i_{L(t)} - I_0$ , from previous result we have



$$\Rightarrow \Delta V_o = \frac{Q}{C} = \frac{1/2 \cdot \frac{\Delta i_L}{2} \cdot T_s/2}{C}$$

$$= \frac{\Delta i_L}{8C f_{sw}} = \frac{24 \text{ V}}{8(500 \cdot 10^6) \cdot 20 \cdot 10^{-3}}$$

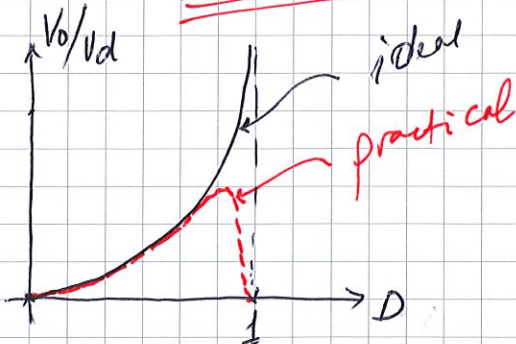
$$\Rightarrow \Delta V_o = \underline{\underline{0.030 \text{ V}}}$$

$\Delta V_o \ll V_o \Rightarrow$  the filters (L & C) are designed well!

Q#3. 
$$V_L = \frac{1}{T_s} \int_0^{T_s} V_L dt = \frac{1}{T_s} \int_0^{DT_s} V_d dt + \frac{1}{T_s} \int_{DT_s}^{T_s} (V_d - V_o) dt = 0$$

↑ switch on  
↑ switch off  
↑ CCM

$$\Rightarrow \frac{V_o}{V_d} = \frac{1}{1-D} \text{ (ideal converter)}$$



Due to the parasitic elements in the converter, the expression  $\frac{V_o}{V_d} = \frac{1}{1-D}$  is not followed for a practical converter.

Q#4. For DCM, energy stored in  $L_m$  is transferred to the  
(a) load

$$\Rightarrow \frac{1}{2} L_m (\hat{\Delta i_m})^2 = \frac{V_o^2}{R_{load}} \cdot T_s$$

(energy exchange in one switch cycle)

$$\Rightarrow \frac{1}{2} L_m (\hat{\Delta i_m})^2 = \frac{V_o^2}{f_{sw} R_{load}}$$

when the switch  $S$  is on,  $v_1 = V_d = L_m \frac{\Delta i_m}{DT_s}$

$$\Rightarrow \hat{\Delta i_m} = \frac{DT_s \cdot V_d}{L_m} = \frac{DV_d}{f_{sw} L_m}$$

$$\frac{1}{2} L_m \left\{ \frac{DV_d}{f_{sw} L_m} \right\}^2 = \frac{V_o^2}{f_{sw} R_{load}}$$

$$\Rightarrow \frac{V_o}{V_d} = \sqrt{\frac{R_{load}}{2L_m f_{sw}}} \cdot D$$

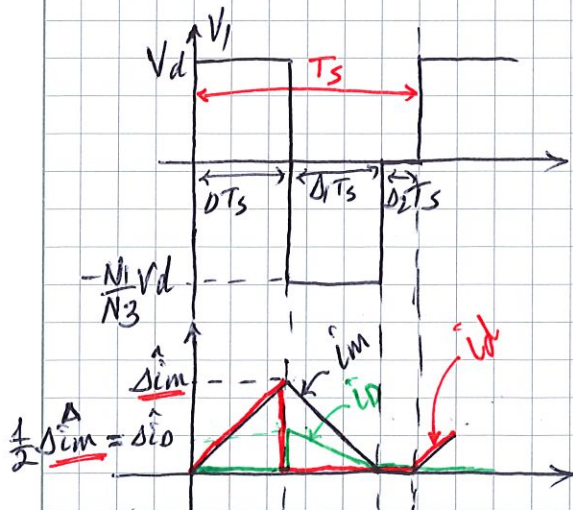
(b) During on,  $v_1 = V_d$ ,  $i_d = i_m$ ,  $i_o = 0$

During off,  $v_3 = -V_o \Rightarrow v_1 = -\frac{N_1}{N_3} V_o$  until  $i_m = 0$  /  $i_d = 0$   
 $i_m = i_o \cdot \frac{N_3}{N_1}$

$v_3 = v_1 = 0$  when  $i_m = 0 = i_o = i_d$

the above expression is for no current in  $N_2$

$\Rightarrow V_o$  remains within the maximum voltage of  $\frac{N_3}{N_2} V_d = 2V_d$



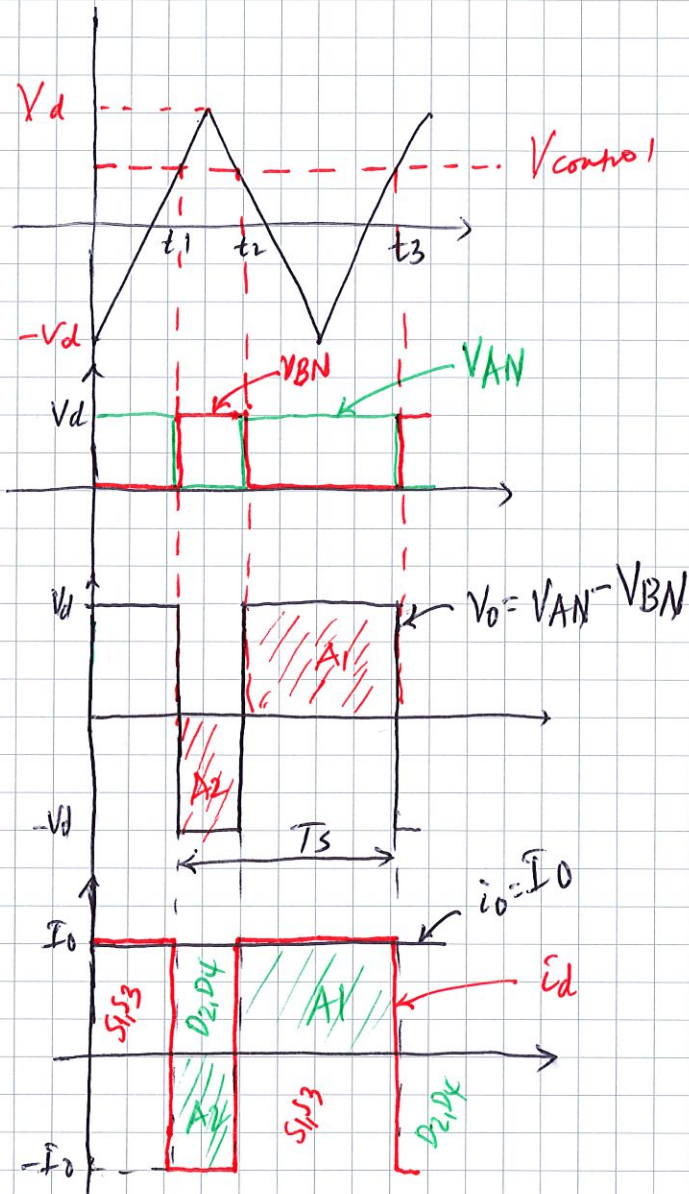
(c) if  $R_{load} \rightarrow \infty \Rightarrow V_o \rightarrow$  very high  
from results of part (a)

$\Rightarrow$  when  $V_o > \frac{N_3}{N_2} V_d$ ,  $D_2$  will be forward biased which provides a path for the demagnetization

$\Rightarrow$  Diode  $D$  will be reverse biased and  $V_o$  will be limited at  $\frac{N_3}{N_2} V_d$

Q#5.

(a)



$$(b) \quad V_o = \frac{A_1 + A_2}{T_s} = V_{control} = \underline{\underline{10V}}$$

$$I_d = \frac{A_1 + A_2}{T_s} : \text{but from } 100\% \text{ efficiency}$$

$$P_{in} = V_o I_d = V_o I_o = 10(5) \Rightarrow \underline{\underline{I_d = 2.5A}}$$

(c)  $t_1 \leq t \leq t_2$ ,  $V_{control} < V_{tri} \Rightarrow S_{2, S4}$  on; due to positive current  $i_o$   
 $\underline{\underline{D_2, D_4}}$  are conducting.

$t_2 \leq t \leq t_3$ ,  $V_{control} > V_{tri} \Rightarrow S_{1, S3}$  on; due to positive current  $i_o$   
 $\underline{\underline{S_1, S3}}$  are conducting.